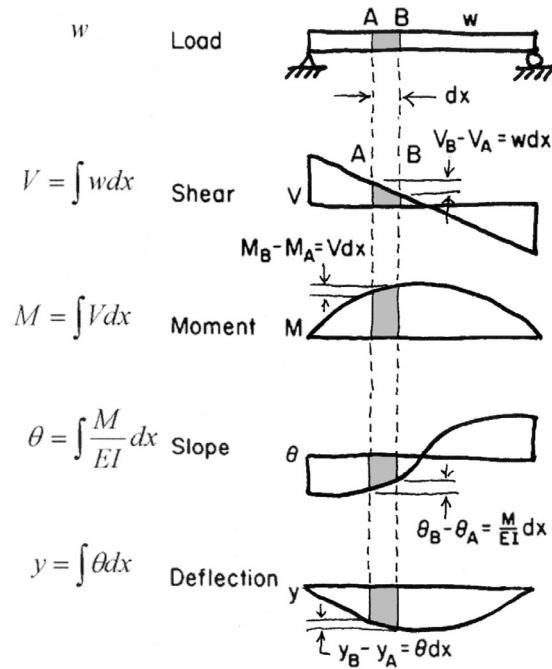


## Bending and Shear in Simple Beams

### Part 2

- Diagrams by Areas (Semi-graphical)
- Diagrams by Equations
- Examples in Form (catenary curves)

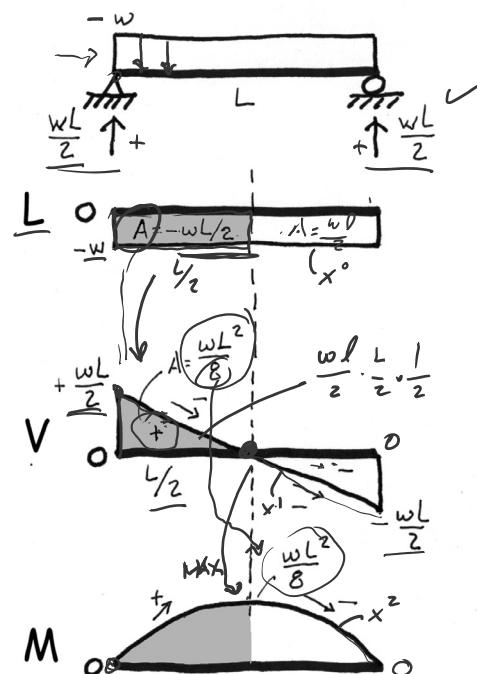


### 3. Shear and Moment by Semi-graphical Method – diagram relationships

By recognizing the diagrammatic relationships between curves and their derivatives and integrals, shear and moment diagrams can be constructed based on areas and slopes of those curves.

#### Moving from Upper to Lower Diagrams:

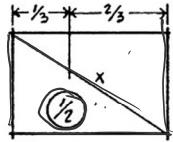
- The area between any two points on the upper diagram is equal to the change in value between same points on the lower diagram.
- The degree of the curve increases by one for each diagram.
- The value on the upper diagram is equal to the slope of the lower diagram.
- Where the upper diagram crosses 0 on the axis, the lower diagram is at a maximum or minimum.
- Points of inflection or “contraflexure” (between + and – curvature) on the elastic curve (deflected shape) are points of zero moment.



### 3. Semi-graphical Method

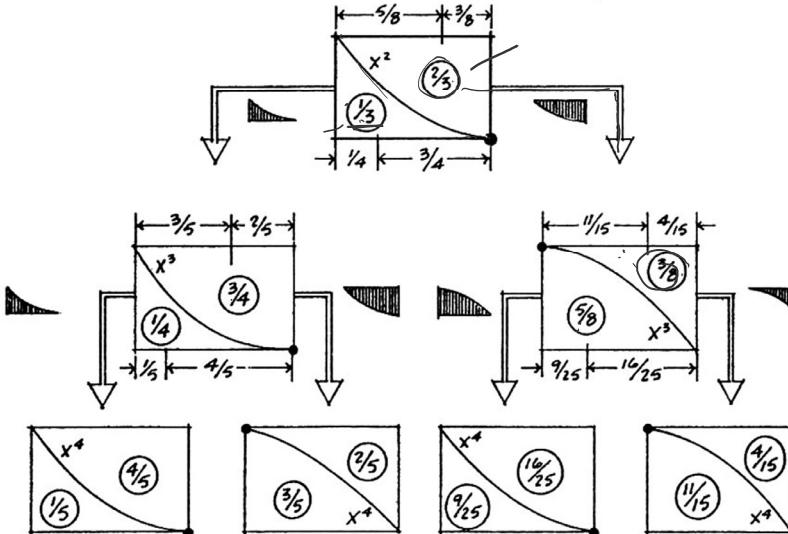
#### FRACTIONAL AREAS OF ENCLOSURE RECTANGLES

CURVES TANGENT TO  
HORIZONTAL AT VERTEX •  
NOTE REVERSE POSSIBILITIES



FRACTION OF RECTANGULAR  
AREAS SHOWN →

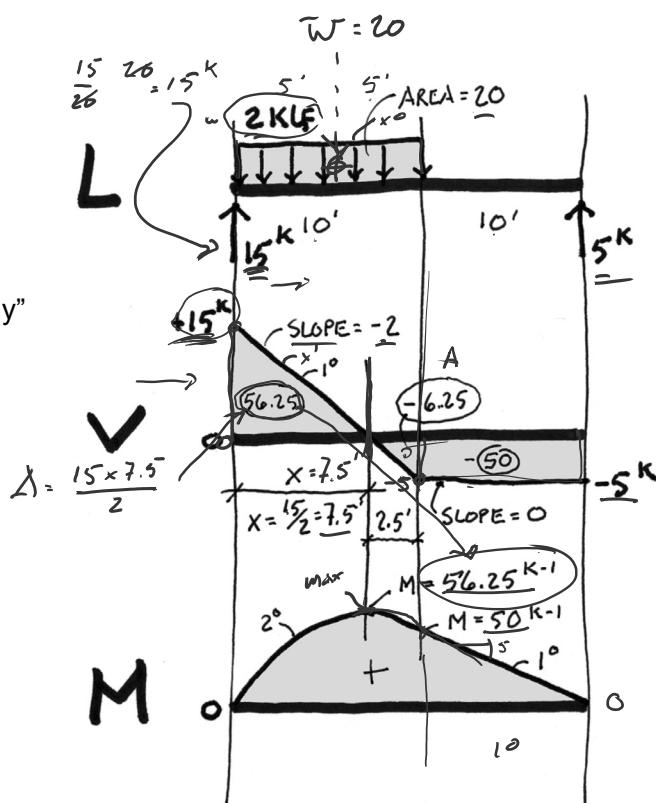
CENTROID OF FRACTIONAL AREA  
LOCATED BY HORIZONTAL  
DIMENSIONS



### 3. Semi-graphical Method

#### Procedure:

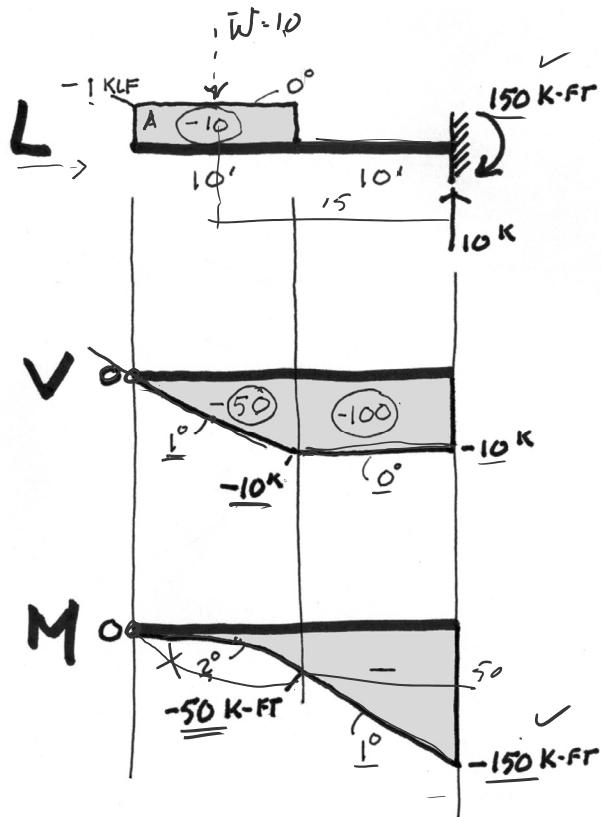
1. Find end reactions
2. Start at left end of V-Diagram and "apply" load from left to right
3. Calculate areas of V-Diagram
4. Find max. and min. values on M-Diagram using V-Diagram areas between axis crossings.
5. Check slope and + or - values



### 3. Semi-graphical Method

example

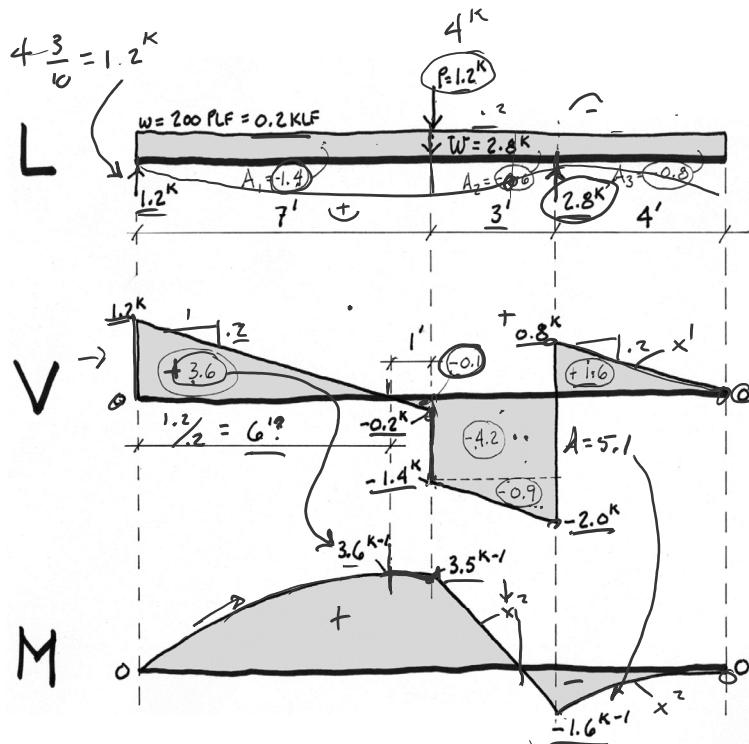
Cantilever Beam



### 3. Semi-graphical Method

example

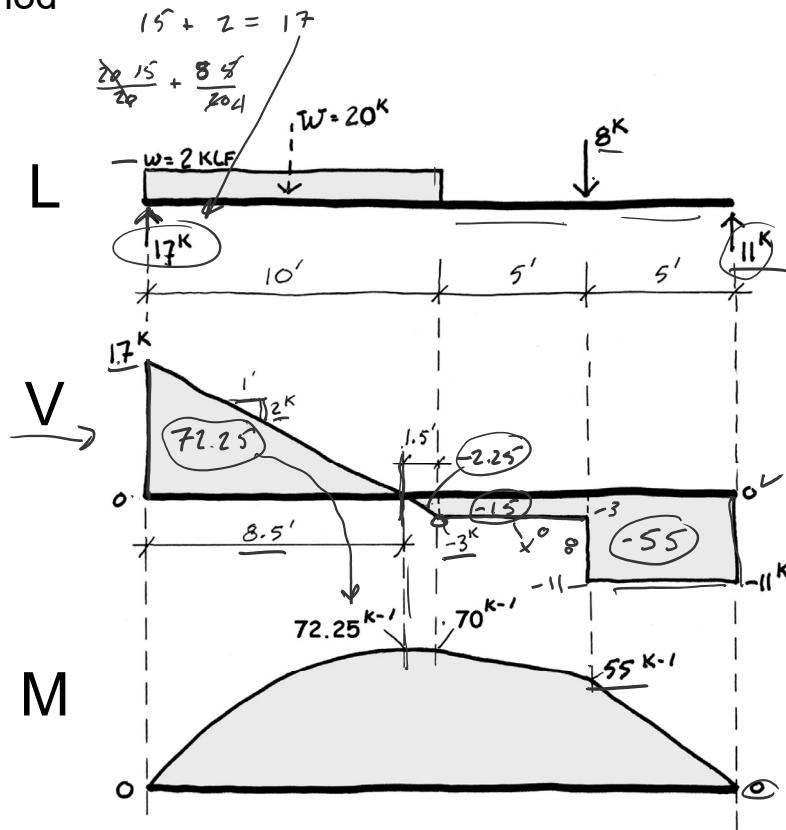
Beam with cantilever



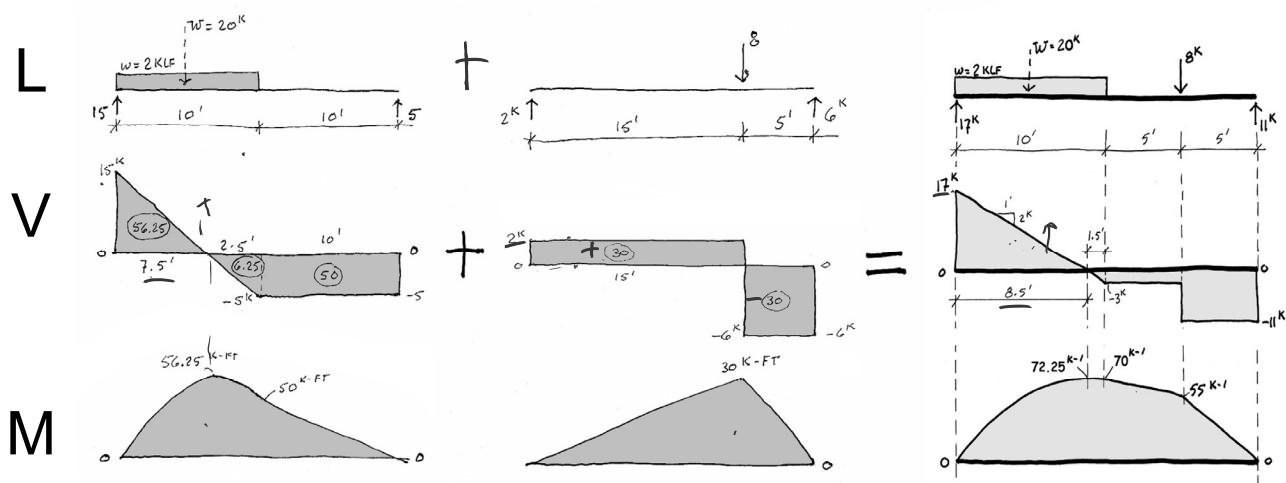
### 3. Semi-graphical Method

example

Simple beam



### 3. Semi-graphical Method - Superposition



# Equations Method

For simple spans:

$V_{max}$  is the larger reaction

For symmetric loadings:

$M_{max}$  is at C.L.

For cantilevers:

Both  $V_{max}$  and  $M_{max}$  are at the support

	<b>1. SIMPLE BEAM—UNIFORMLY DISTRIBUTED LOAD</b> Total Equiv. Uniform Load . . . . . $= wl$ $R = V$ . . . . . $= \frac{wl}{2}$ $V_x$ . . . . . $= w \left( \frac{l}{2} - x \right)$ $M_{max}$ (at center) . . . . . $= \frac{wl^2}{8}$ $M_x$ . . . . . $= \frac{wx}{2} (l - x)$ $\Delta_{max}$ (at center) . . . . . $= \frac{5wl^4}{384EI}$ $\Delta_x$ . . . . . $= \frac{wx}{24EI} (l^3 - 2lx^2 + x^3)$
	<b>2. SIMPLE BEAM—LOAD INCREASING UNIFORMLY TO ONE END</b> Total Equiv. Uniform Load . . . . . $= \frac{16W}{9\sqrt{3}} = 1.0264W$ $R_1 = V_1$ . . . . . $= \frac{W}{3}$ $R_2 = V_2$ max . . . . . $= \frac{2W}{3}$ $V_x$ . . . . . $= \frac{W}{3} - \frac{Wx^2}{l^2}$ $M_{max}$ (at $x = \frac{l}{\sqrt{3}} = .5774l$ ) . . . . . $= \frac{2wl}{9\sqrt{3}} = .1283wl$ $M_x$ . . . . . $= \frac{Wx}{3l^2} (l^2 - x^2)$ $\Delta_{max}$ (at $x = l\sqrt{1 - \frac{8}{15}} = .5193l$ ) . . . . . $= 0.0130 \frac{wl^3}{EI}$ $\Delta_x$ . . . . . $= \frac{Wx}{180EI/l^2} (3x^4 - 10l^2x^2 + 7l^4)$
	<b>7. SIMPLE BEAM—CONCENTRATED LOAD AT CENTER</b> Total Equiv. Uniform Load . . . . . $= 2P$ $R = V$ . . . . . $= \frac{P}{2}$ $M_{max}$ (at point of load) . . . . . $= \frac{Pl}{4}$ $M_x$ (when $x < \frac{1}{2}$ ) . . . . . $= \frac{Px}{2}$ $\Delta_{max}$ (at point of load) . . . . . $= \frac{Pl^3}{48EI}$ $\Delta_x$ (when $x < \frac{1}{2}$ ) . . . . . $= \frac{Px}{48EI} (3l^2 - 4x^2)$

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Structures I

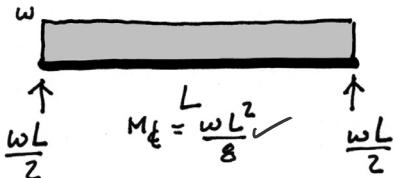
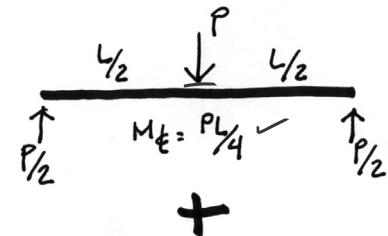
Slide 9 of 14

## 4. Superposition of Equations

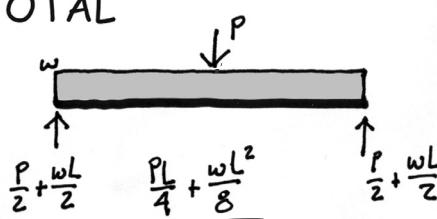
Equations of shear or moment may be combined (superimposed) for any number of cases.

BUT

The appropriate location along the beam for which the equation is valid must be maintained



TOTAL



Thus

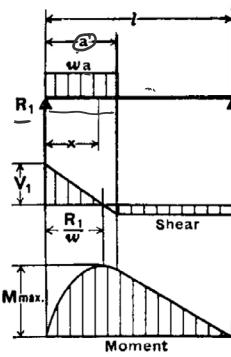
At the reaction,  $V = P/2 + wL/2$

And at the C.L.  $M = PL/4 + WL^2/8$

## Non-symmetric

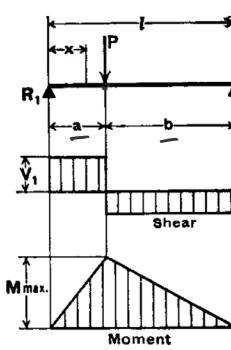
For more complex loads, care must be taken to combine equations at the same location or point on the beam ( $x$ ).

### 5. SIMPLE BEAM—UNIFORM LOAD PARTIALLY DISTRIBUTED AT ONE END



$$\begin{aligned}
 R_1 &= V_1 \text{ max.} & = \frac{w(a)}{2l}(2l-a) \\
 R_2 &= V_2 & = \frac{wa^2}{2l} \\
 V_x & \quad (\text{when } x < a) & = R_1 - wx \\
 M \text{ max.} & \quad (\text{at } x = \frac{R_1}{w}) & = \frac{R_1^2}{2w} \\
 M_x & \quad (\text{when } x < a) & = R_1x - \frac{wx^2}{2} \\
 M_x & \quad (\text{when } x > a) & = R_2(l-x) \\
 \Delta x & \quad (\text{when } x < a) & = \frac{wx}{24EI_l} (a^2(2l-a)^2 - 2ax^2(2l-a) + lx^3) \\
 \Delta x & \quad (\text{when } x > a) & = \frac{wa^2(l-x)}{24EI_l} (4xl - 2x^2 - a^2)
 \end{aligned}$$

### 8. SIMPLE BEAM—CONCENTRATED LOAD AT ANY POINT



$$\begin{aligned}
 \text{Total Equiv. Uniform Load} & = \frac{8Pab}{l^2} \\
 R_1 &= V_1 \text{ (max. when } a < b) & = \frac{Pb}{l} \\
 R_2 &= V_2 \text{ (max. when } a > b) & = \frac{Pa}{l} \\
 M \text{ max.} & \quad (\text{at point of load}) & = \frac{Pab}{l} \\
 M_x & \quad (\text{when } x < a) & = \frac{Pbx}{l} \\
 \Delta \text{max.} & \quad (\text{at } x = \sqrt{\frac{a(a+2b)}{3}} \text{ when } a > b) & = \frac{Pab(a+2b)\sqrt{3a(a+2b)}}{27EI_l} \\
 \Delta a & \quad (\text{at point of load}) & = \frac{Pab^2}{3EI_l} \\
 \Delta x & \quad (\text{when } x < a) & = \frac{Pbx}{6EI_l} (l^2 - b^2 - x^2)
 \end{aligned}$$

## 4. Superposition of Equations - example

find  $x$  at  $M_{\max}$  for combined asymmetric cases

END REACTIONS (NOTE: VARIABLES DIFFER IN DIFFERENT EQUATIONS)

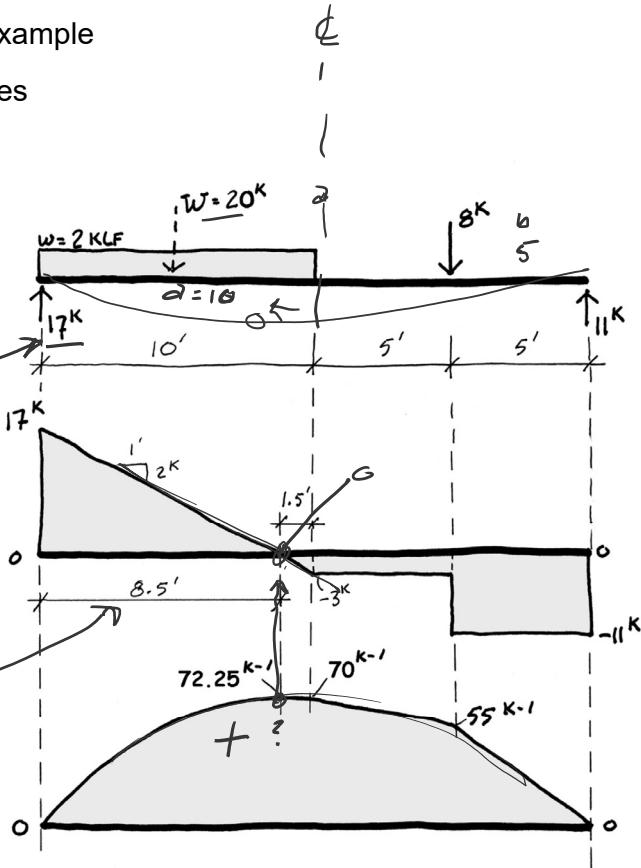
$$\begin{aligned}
 R_L &= \frac{w a^2}{2 l^2} (2l-a)^2 + \frac{Pb}{l} \\
 R_L &= \frac{2(10)}{2(20)} (2(20)-10) + \frac{8(5)}{20} b \\
 R_L &= 15 + 2 = 17 \text{ K}
 \end{aligned}$$

MOMENT EQUATIONS AT X

$$M_x = R_1 x - \frac{w x^2}{2} + \frac{Pbx}{l}$$

To FIND  $x$ : DIFFERENTIATE AND SOLVE AT 0 (M max)

$$\begin{aligned}
 R_1 - wx &+ \frac{Pb}{l} \\
 15 - 2x + 2 &= 0 \\
 x &= 8.5' \\
 \text{AND} \quad M_{\max} &= 15(8.5) - \frac{2(8.5)^2}{2} + \frac{8(5)(8.5)}{20} \\
 M_{\max} &= 55.25 + 17 = 72.25 \text{ K'-l}
 \end{aligned}$$

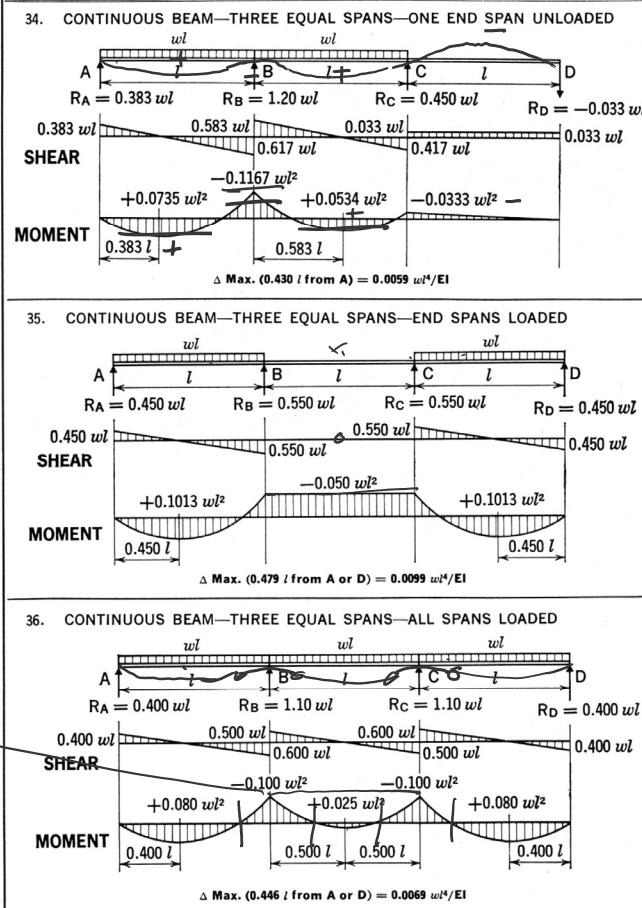


## Simple vs. Continuous Beams

- Simple Beam
  - End moments = 0  $\frac{w l^2}{8} = .125 w l^2$
  - when symmetric,  $M_{max}$  at C.L.  
e.g.  $wL^2/8 = 0.125wL^2$
- Continuous Beam
  - Exterior end moments = 0
  - Interior support moments are usually negative
  - Mid-span moments are usually positive
  - End + Mid =  $0.125wL^2$



Note: moments shown reversed



## Moment Diagram vs. Catenary Curve

For a gravity loaded simple span beams, the shape of the moment diagram is the inverse of the catenary curve.

